

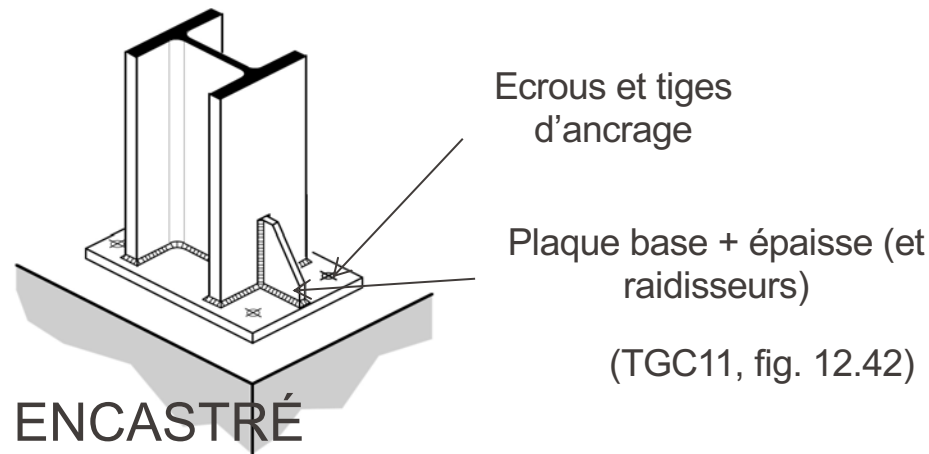
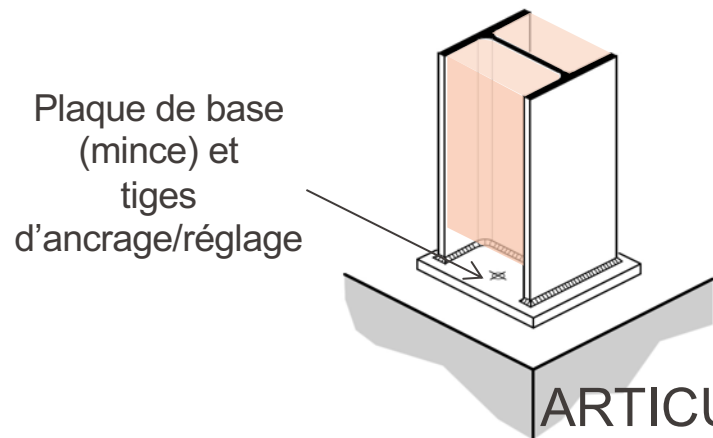


Pieds de poteaux (ou montants) (réf. TGC 11, section 12.6)

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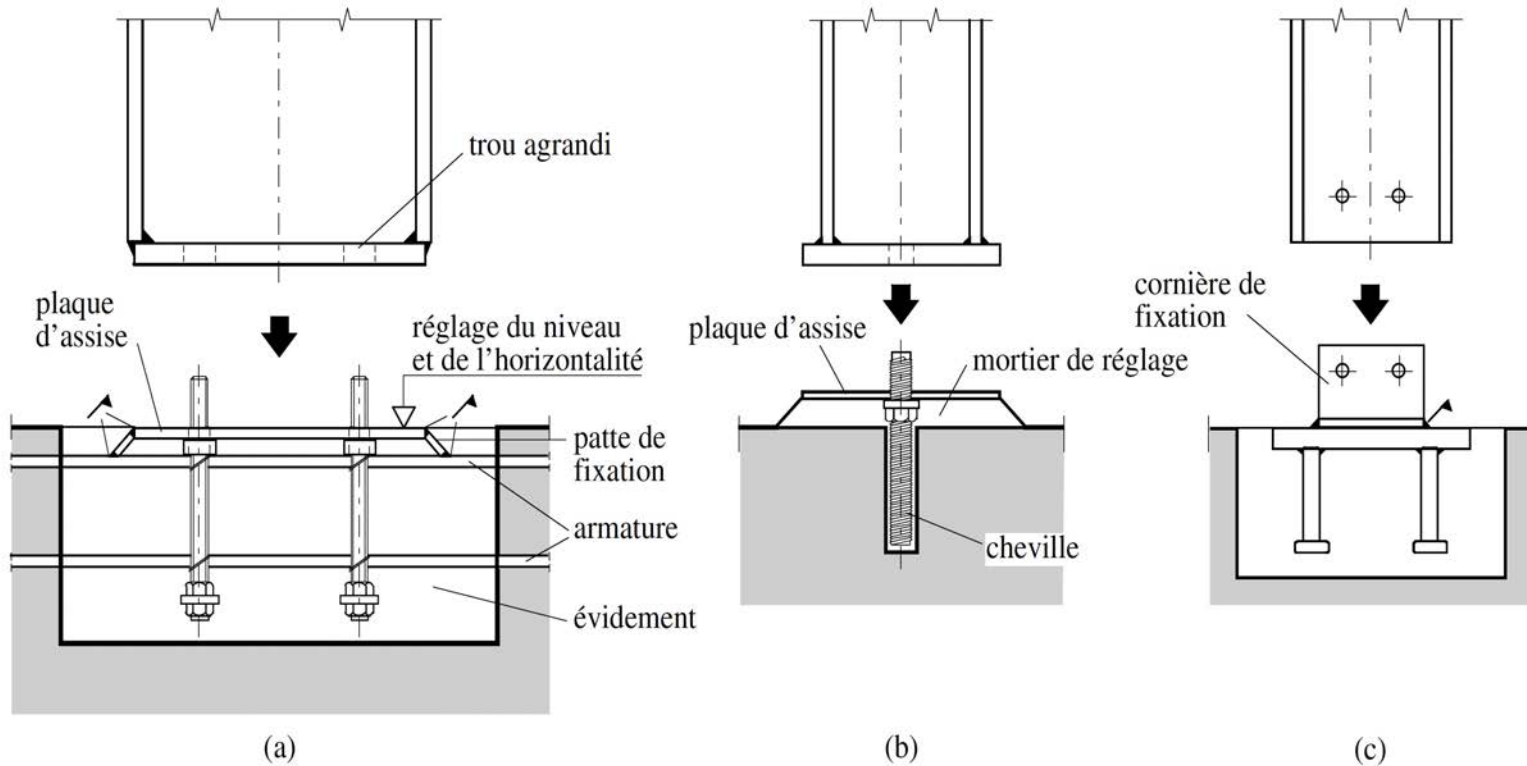
- Principes
- Transmission des efforts dans le béton
- Pieds de montants articulés
- Pieds de montants encastrés
- Exemples constructifs

- Poteau, métalliques ou mixtes, généralement muni d'une base
- Posé sur massif de fondation
- Fixé à la fondation par tige(s) d'ancrage (maintien en position, contre soulèvement, reprise V et si besoin M)
- Avec système réglage pour reprise tolérances (trous oblongs, écrous réglage vertical, espace de scellement, etc.)



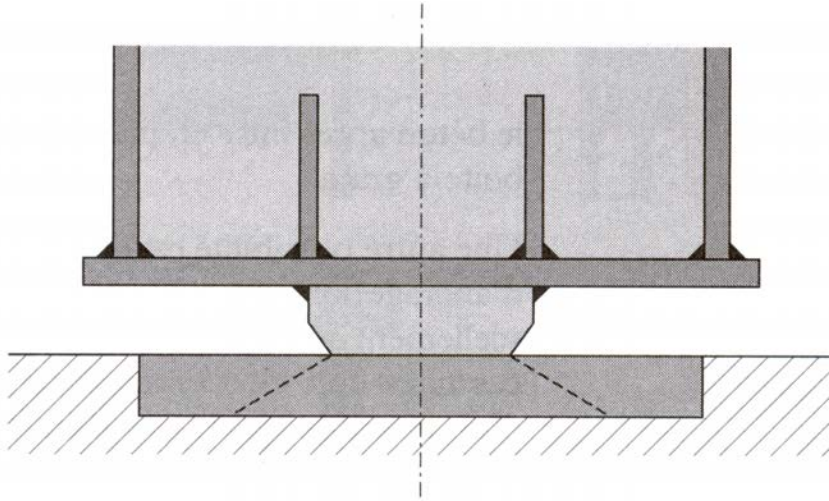
(TGC11, fig. 12.42)

TGC11, fig. 12.43: Principes, pieds articulés

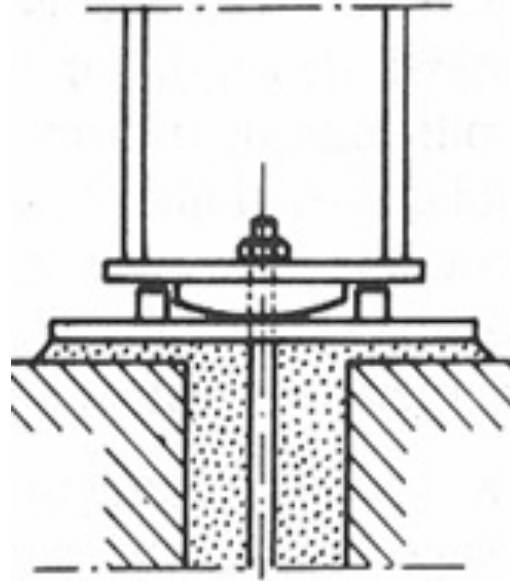


Positionnement précis: plaque d'assise permet des ajustements

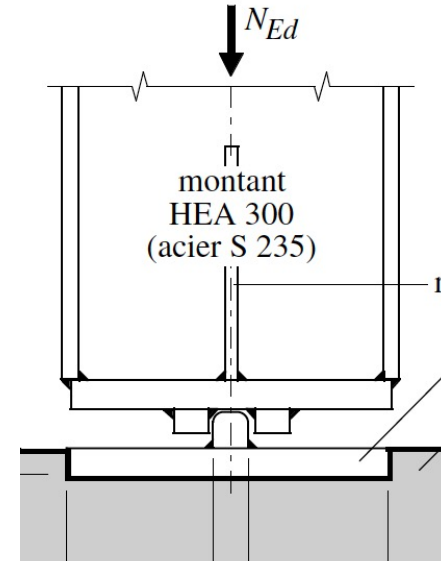
Principes, pieds articulés



Pied de poteau avec grain d'appui

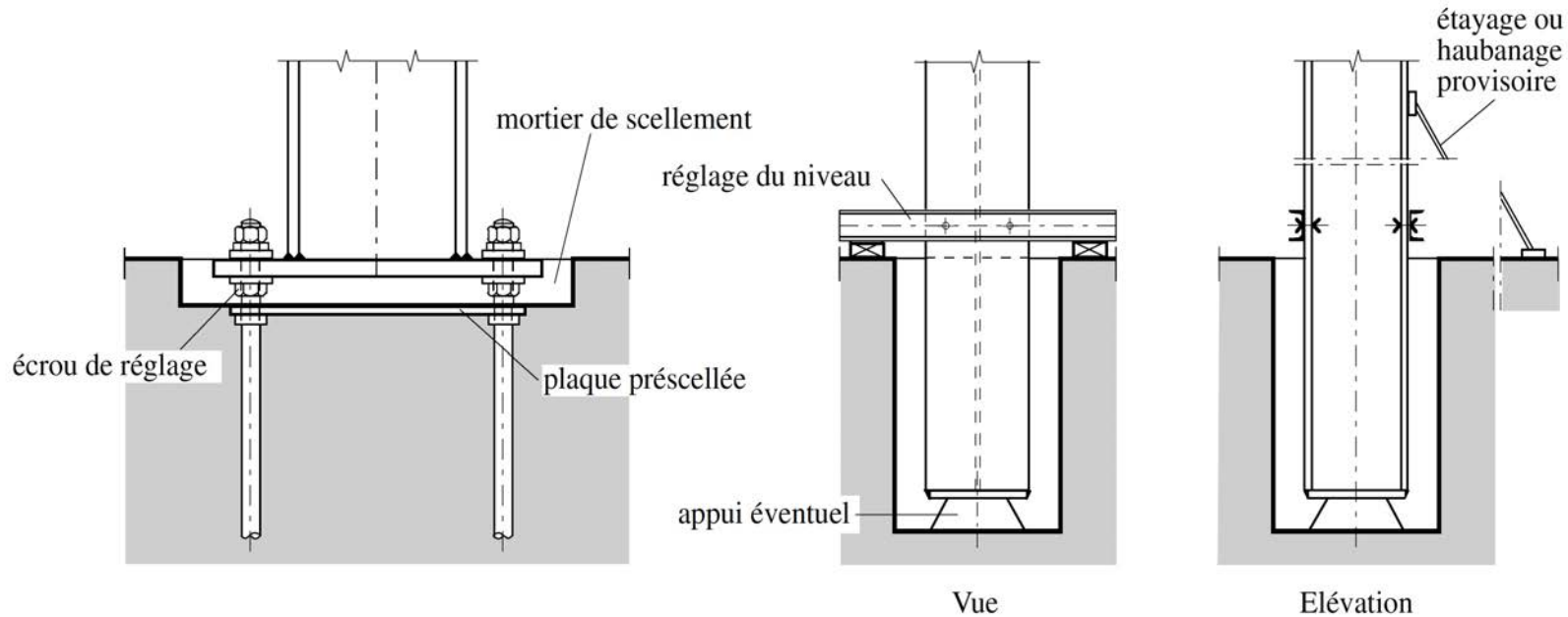


TGC11, fig. 12.57



Si poteau trop important, pour permettre rotation, plaque intermédiaire étroite ou grain d'appui

TGC11, fig. 12.44: Principes, pieds encastrés



(a)

Halles et bâtiments jusqu'à 15m

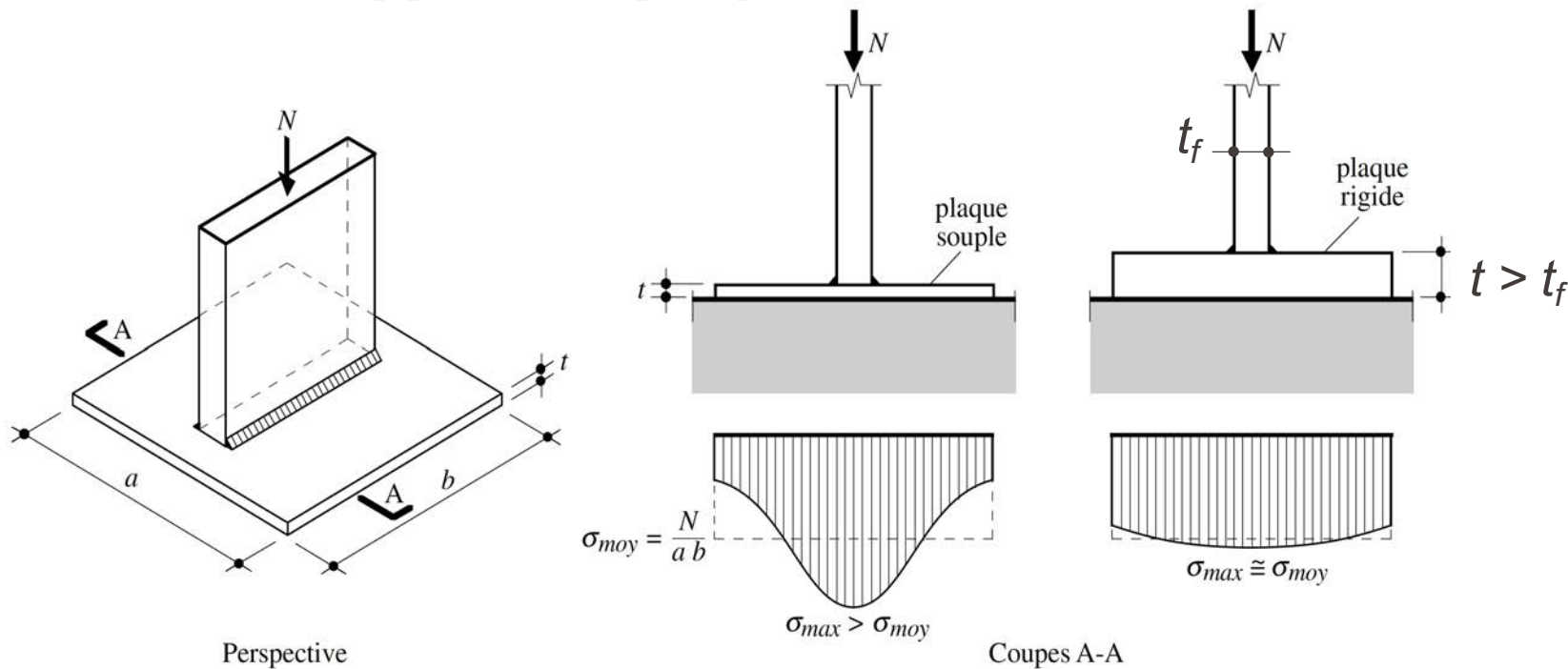
(b)

Souvent recommandé pour bâtiments plus élevés, plus gros profilés/efforts

Positionnement précis: plus exigeant, exemples de procédures de mise en place

TGC11, fig. 12.45: transmission efforts dans béton.

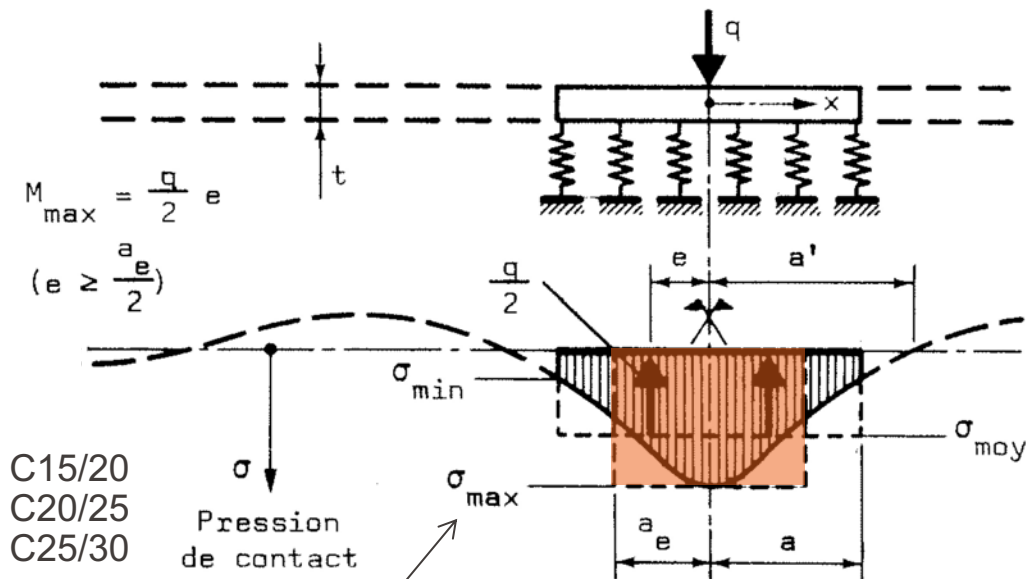
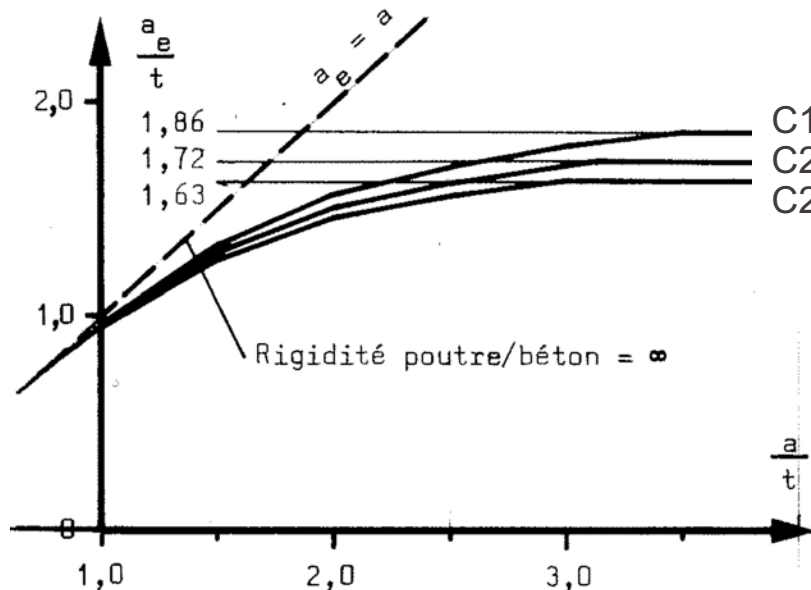
Pression d'appui sous plaque de base



Plaque rigide: meilleure répartition des contraintes

Distrib. élast. = $f(E_b, E_a, t, \text{dimensions fondation, etc.})$

Largeur surface portante a_e (modèle plast.)
= $f(f_{cd}, f_{yd}, t, \text{dimensions fondation, etc.})$



Fct résistance du
béton et de son
confinement

$a_e = d$
se mesure depuis
les faces des
éléments du poteau

Surface portante efficace
selon EC 3:

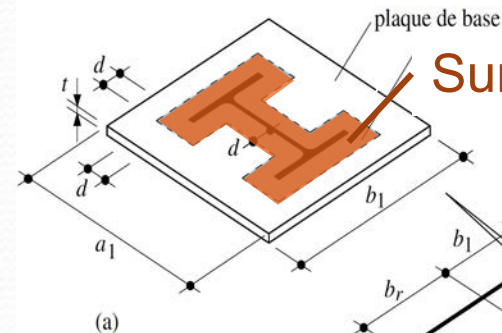
$$d = t \cdot \sqrt{\frac{f_{yd}}{2 \cdot k_c \cdot f_{cd}}}$$

où

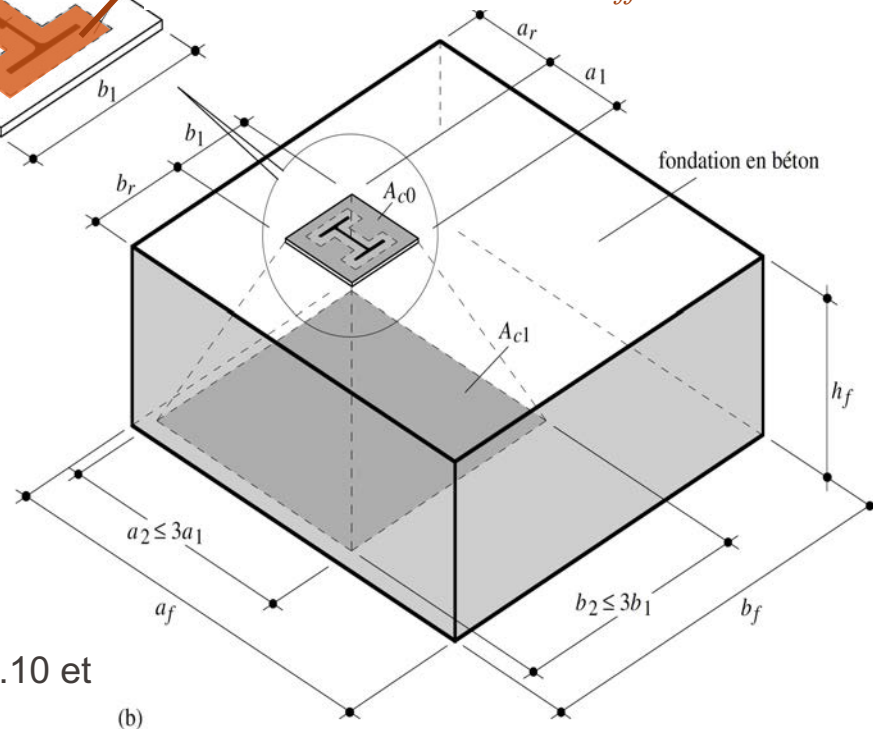
$$k_c = \sqrt{\frac{A_{c1}}{A_{c0}}} = \sqrt{\frac{a_2 \cdot b_2}{a_1 \cdot b_1}} \leq 3$$

k_c : Facteur de concentration
ou plus correct de confinement

EN 1992-1-1: 2004 § 6.7.8 (2) et
EN 1993-1-8: 2005 § 6.2.5



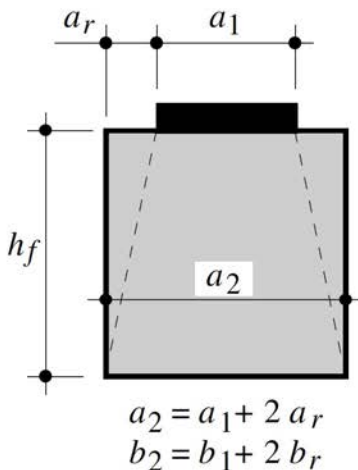
Sous effort NORMAL
Surface portante A_{eff} ($\sigma = cte$)



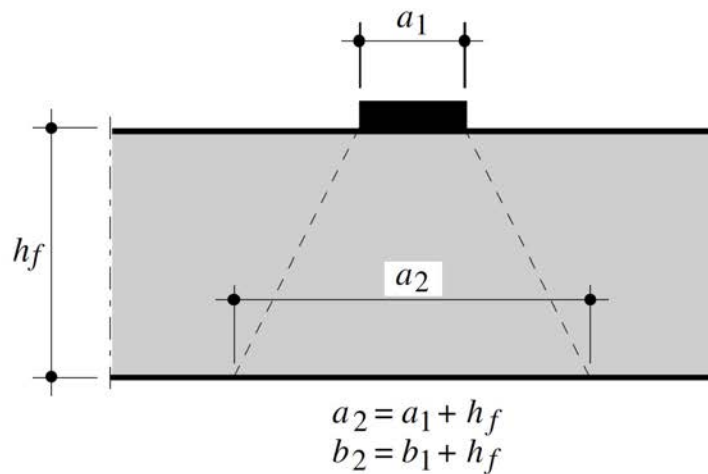
SIA 262 § 4.2.1.10 et
SIA 263 § 6.8

Fig. 12.47: Types de fondation et valeurs k_c

Trapue (- confinement)



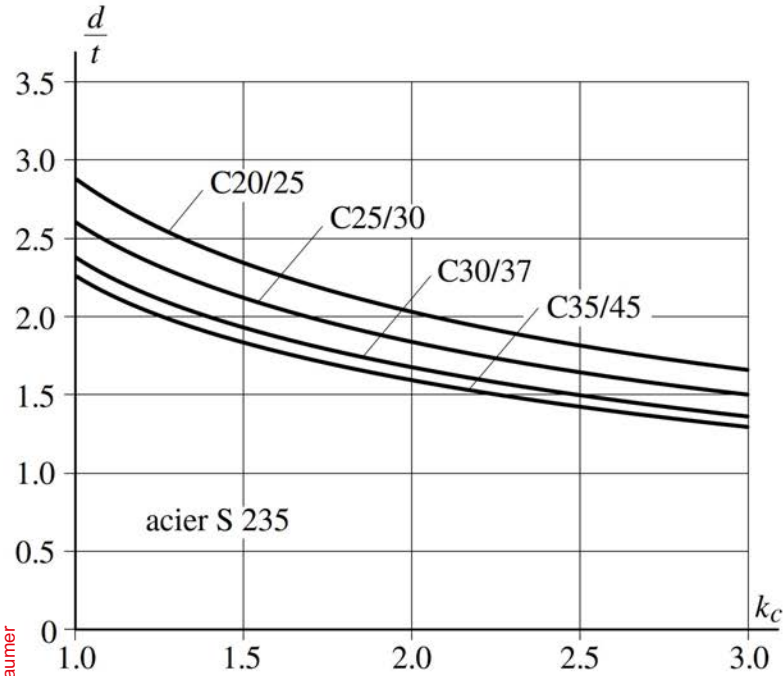
Elancée (+ confinement)



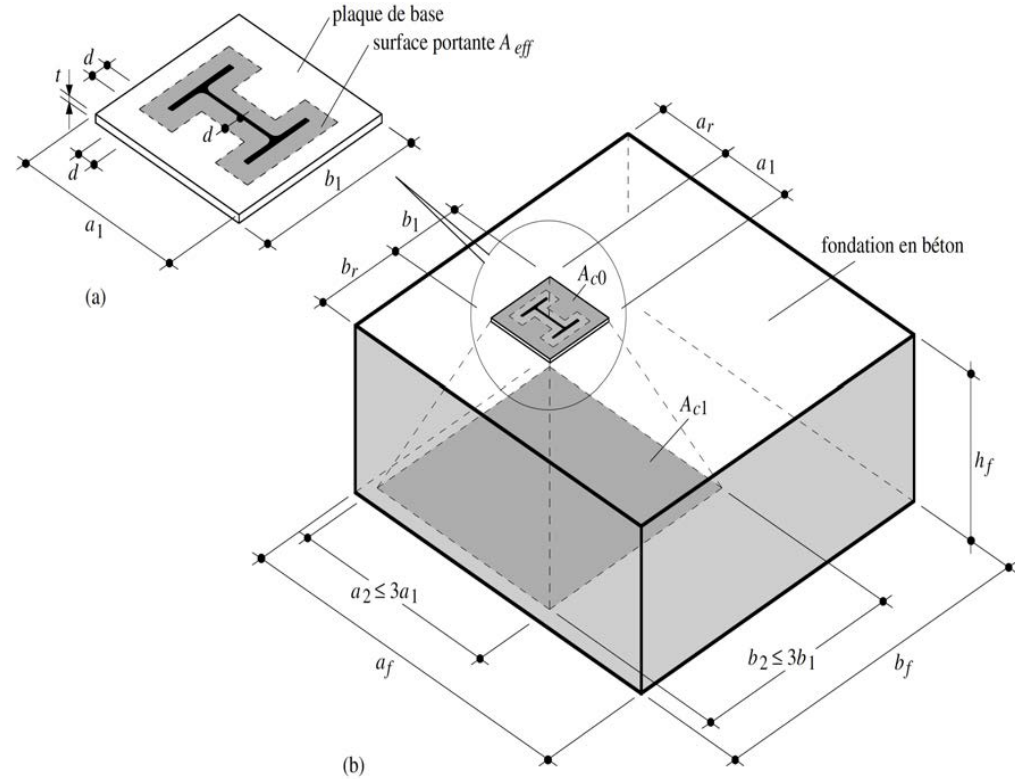
$$k_c = 1.0 \text{ à } 2.0$$

$$k_c = 2.0 \text{ à } 3.0$$

Note: vérifier limites d'applicabilité



$$k_c = \sqrt{\frac{A_{c1}}{A_{c0}}}$$



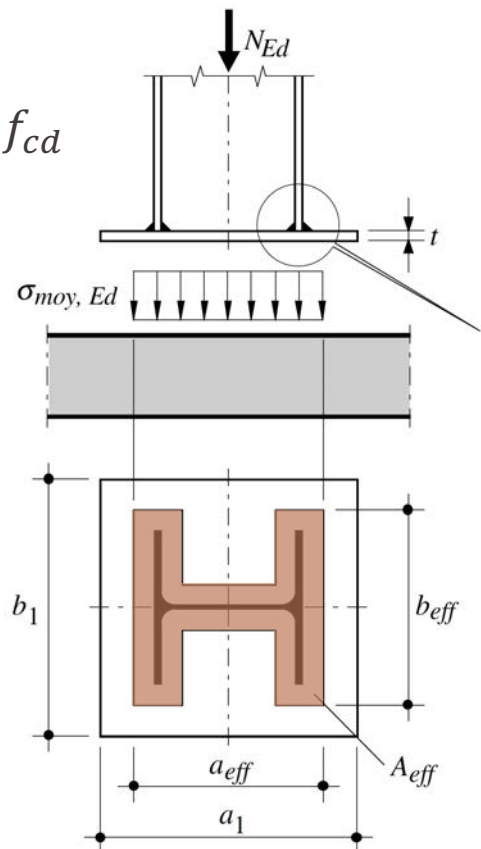
Béton:

$$\sigma_{moy,Ed} = \frac{N_{Ed}}{A_{eff}} \leq \sigma_{c,Rd} = k_c \cdot \beta_j \cdot f_{cd}$$

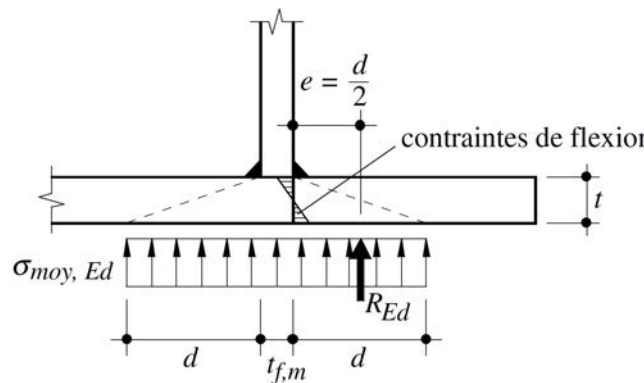
Plaque: $M_{Ed} = R_{Ed} \cdot e \leq \frac{M_{el}}{\gamma_a}$

ou

$$R_{Ed} = \sigma_{moy,Ed} \cdot d \cdot b_{eff}$$



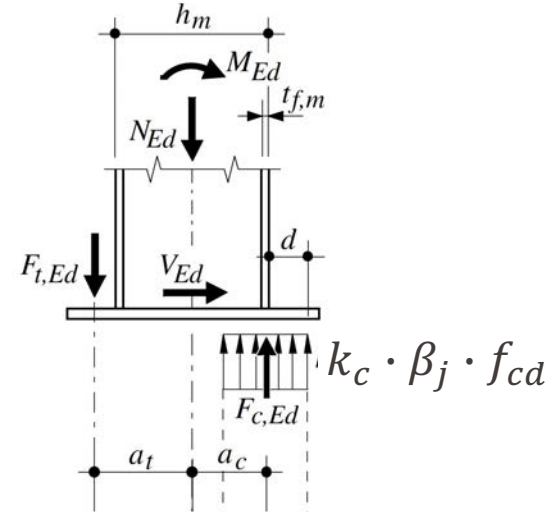
(a) Compression sur le béton



(b) Flexion de la plaque

(TGC 11, fig. 12.49)

$$\sum M = 0 \rightarrow M_{Ed} - F_{t,Ed} \cdot a_t - F_{c,Ed} \cdot a_c = 0$$

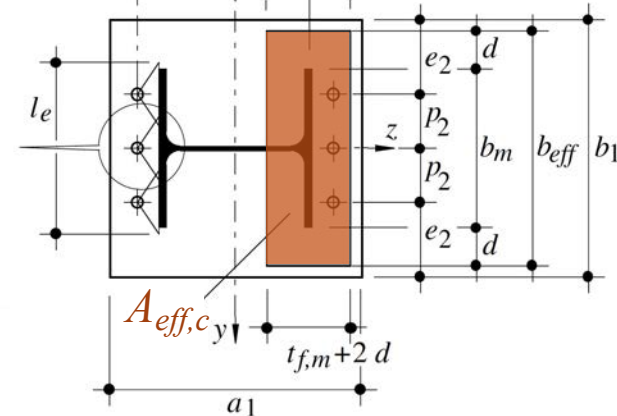
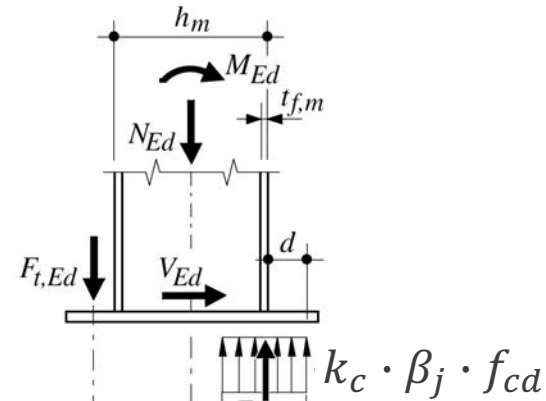
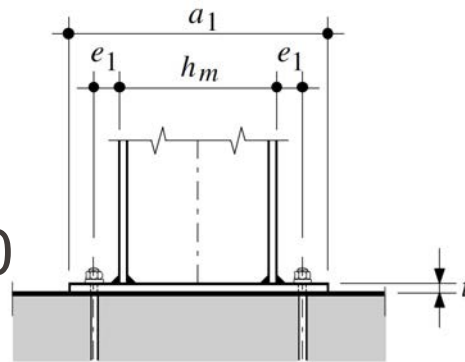


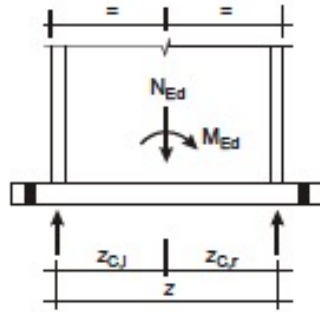
$$\sum N = 0 \rightarrow N_{Ed} + F_{t,Ed} - F_{c,Ed} = 0$$

$$\sum M = 0 \rightarrow M_{Ed} - F_{t,Ed} \cdot a_t - F_{c,Ed} \cdot a_c = 0$$

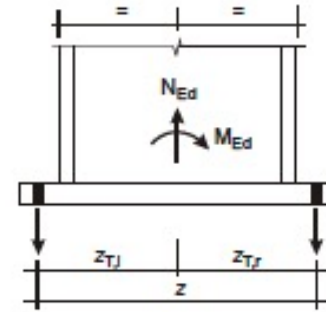
Vérifications:

- Béton: $F_{c,Ed} \leq k_c \cdot \beta_j \cdot f_{cd} \cdot A_{eff,c}$
- Tiges: $F_{t,Ed} \leq n \cdot F_{t,Rd}$
- Flexion plaque, côté comprimé et tendu

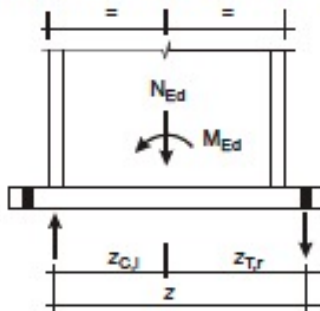




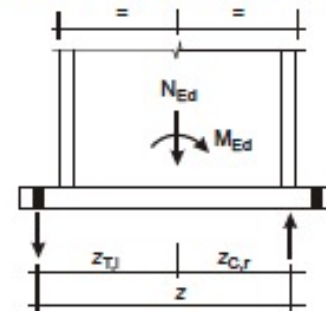
a) Assemblage de pied de poteau dans le cas d'un effort normal de compression dominant



b) Assemblage de pied de poteau dans le cas d'un effort normal de traction dominant



c) Assemblage de pied de poteau dans le cas d'un moment fléchissant dominant



d) Assemblage de pied de poteau dans le cas d'un moment fléchissant dominant



Merci

Prof. A. Nussbaumer
RESSLab

Gare d'Aveiro, Photo A. Nussbaumer

Annexe: exemples constructifs

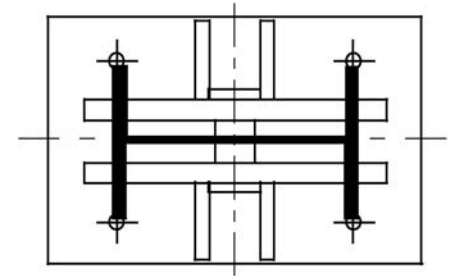
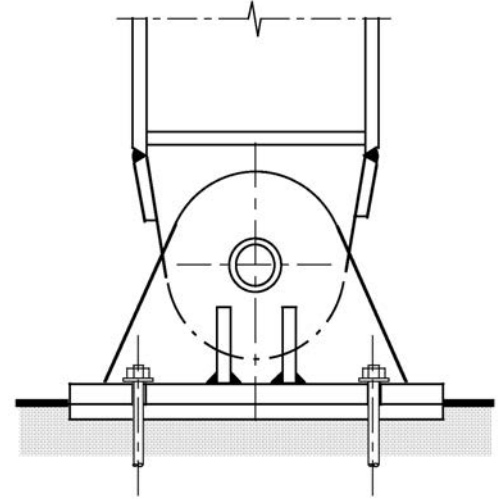


Photo entête chapitre 11 du TGC 11. Halle de sport Buchholz



UNIL, Extranef, photo A. Nussbaumer



UNIL, Extranef, photo A. Nussbaumer



UNIL, Extranef, photo A. Nussbaumer



Fabrication, ateliers Sottas SA, photo A. Nussbaumer